



International Institute for
Applied Systems Analysis
www.iiasa.ac.at

Optimal Control of Linear Econometric Systems with Inequality Constraints on the Control Variables

Robertson, G.C.

**IIASA Professional Paper
October 1983**



Robertson, G.C. (1983) Optimal Control of Linear Econometric Systems with Inequality Constraints on the Control Variables. IIASA Professional Paper. IIASA, Laxenburg, Austria, PP-83-004 Copyright © October 1983 by the author(s). <http://pure.iiasa.ac.at/2384/> All rights reserved. Permission to make digital or hard copies of all or part of this work for personal or classroom use is granted without fee provided that copies are not made or distributed for profit or commercial advantage. All copies must bear this notice and the full citation on the first page. For other purposes, to republish, to post on servers or to redistribute to lists, permission must be sought by contacting repository@iiasa.ac.at

NOT FOR QUOTATION
WITHOUT PERMISSION
OF THE AUTHOR

**OPTIMAL CONTROL OF
LINEAR ECONOMETRIC SYSTEMS
WITH INEQUALITY CONSTRAINTS
ON THE CONTROL VARIABLES**

Gerald C. Robertson

October 1983

PP-83-4

Professional Papers do not report on work of the International Institute for Applied Systems Analysis, but are produced and distributed by the Institute as an aid to staff members in furthering their professional activities. Views or opinions expressed are those of the author(s) and should not be interpreted as representing the view of either the Institute or its National Member Organizations.

INTERNATIONAL INSTITUTE FOR APPLIED SYSTEMS ANALYSIS
2361 Laxenburg, Austria

THE AUTHOR

Gerald C. Robertson works for the Marketing and Economics Branch of Agriculture Canada and was with the Food and Agriculture Program at IIASA from April 1982 to June 1983.

**OPTIMAL CONTROL OF
LINEAR ECONOMETRIC SYSTEMS
WITH INEQUALITY CONSTRAINTS
ON THE CONTROL VARIABLES**

Gerald C. Robertson

Chow (1975, pp. 157) develops a series of methods to solve the following optimal tracking problem.

$$\min(y_t - a_t)'K_t(y_t - a_t)$$

subject to

$$y_t = A_t y_{t-1} + C_t x_t + B_t z_t$$

One of the methods is that of Lagrangian multipliers. K.C. Tan (1979) extends this to include the case where the instruments must satisfy

$$F_t x_t = f_t$$

The purpose of this note is to develop the corresponding solution when the instruments are constrained

$$l_t \leq x_t \leq u_t .$$

With the addition of these constraints the problem becomes

$$\min(y_t - a_t)'K_t(y_t - a_t)$$

subject to

$$y_t = A_t y_{t-1} + C_t x_t + B_t z_t$$

and

$$\begin{aligned} u_t - x_t &\geq 0 & \text{where } u_t > l_t \\ x_t - l_t &\geq 0 \end{aligned}$$

Forming the Lagrangian we get

$$L = \frac{1}{2}(y_t - a_t)'K_t(y_t - a_t) \quad (2)$$

$$\begin{aligned} & - \sum_{t=1}^T \lambda_t'(y_t - A_t y_{t-1} - C_t x_t - B_t z_t) \\ & - \sum_{t=1}^T \rho_t'(u_t - x_t) \\ & - \sum_{t=1}^T \sigma_t'(x_t - l_t) \end{aligned}$$

$$\frac{\partial L}{\partial y_t} = K_t(y_t - a_t) - \lambda_t + A_{t-1}'\lambda_{t-1} = 0 \quad (3)$$

$$\frac{\partial L}{\partial x_t} = C_t'\lambda_t + \rho_t - \sigma_t = 0 \quad (4)$$

$$\frac{\partial L}{\partial \lambda_t} = y_t - A_t y_{t-1} - C_t x_t - B_t z_t = 0 \quad (5)$$

$$\frac{\partial L}{\partial \sigma_t} = -x_t + l_t \leq 0, \quad \sigma_t \frac{\partial L}{\partial \sigma_t} = \sigma_t(-x_t + l_t) = 0 \quad (6)$$

$$\frac{\partial L}{\partial \rho_t} = -u_t + x_t \leq 0, \quad \rho_t \frac{\partial L}{\partial \rho_t} = \rho_t(-u_t + x_t) = 0 \quad (7)$$

If this is a "free endpoint" problem $\lambda_{T+1} = 0$, following Chow (1975), therefore using (3)

$$\begin{aligned} \lambda_T &= K_T y_T - K_T a_T + A_{T+1}' \lambda_{T+1} \\ &= K_T y_T - K_T a_T \end{aligned} \quad (8)$$

or setting $H_T = K_T$ and $h_T = K_T a_T$

$$\lambda_T = H_T y_T - h_T \quad (9)$$

Substitute this into (4)

$$\begin{aligned} C_T' \lambda_T + \rho_T - \sigma_T &= 0 \\ C_T'(H_T y_T - h_T) + \rho_T - \sigma_T &= 0 \end{aligned} \quad (10)$$

$$C'_T H_T y_T - C'_T h_T + \rho_T - \sigma_T = 0$$

Substitute (5) into this

$$C'_T H_T A_T y_{T-1} + C'_T H_T C_T x_t + C'_T H_T B_T z_T - C'_T h_T + C'_T h_T + \rho_T - \sigma_T = 0$$

Solving for x_T

$$\begin{aligned} x_T &= G_T y_{T-1} + g_T + (C'_T H_T G)^{-1}(\rho_T - \sigma_T) \\ &= G_T y_{T-1} + g_T + \rho_T^\bullet - \sigma_T^\bullet \end{aligned} \quad (11)$$

where

$$G_T = -(C'_T H_T C_T)^{-1} C'_T H_T A_T$$

$$g_T = -(C'_T H_T C_T)^{-1} C'_T (H_T - B_T z_T - h_T)$$

$$\rho_T^\bullet = (C'_T H_T C_T)^{-1} \rho_T$$

$$\sigma_t^\bullet = (C'_T H_T C_T)^{-1} \sigma_t .$$

Substituting this into (5) we obtain

$$y_T = (A_T + C_T G_T) y_{T-1} + B_T z_T + C_T g_T + C_T \rho_T^\bullet - C_T \sigma_T^\bullet .$$

Substituting this into (9)

$$\lambda_T = H_T (A_T + C_T G_T) y_{T-1} + H_T (B_T z_T + C_T g_T) + H_T C_T \rho_T^\bullet - H_T C_T \sigma_T^\bullet - h_T \quad (12)$$

Lagging (8)

$$\lambda_{t-1} = K_{t-1} y_{t-1} - K_{t-1} a_{t-1} + A'_t \lambda_t$$

Substituting (12) into it

$$\begin{aligned} \lambda_{t-1} &= K_{t-1} y_{t-1} - K_{t-1} a_{t-1} + A'_t H_t (A_t + C_t G_t) y_{t-1} \\ &\quad + A'_t H_t (B_t z_t + C_t g_t) \\ &\quad + A'_t H_t C_t \rho_t^\bullet - A'_t H_t C_t \sigma_t^\bullet - A'_t h_t \end{aligned} \quad (13)$$

and

$$\lambda_{t-1} = H_{t-1} y_{t-1} - h_{t-1}$$

where

$$\begin{aligned} H_{t-1} &= K_{t-1} + A'_t H_t (A_t + C_t G_t) \\ h_{t-1} &= K_{t-1} a_{t-1} - A'_t H_t (B_t z_t + C_t g_t + C_t \rho_t^* - C_t \sigma_t^*) + A'_t h_t \end{aligned} \quad (14)$$

There are three possibilities in any given year.

$$A. \quad l_t < x_t < u_t$$

Chow's unconstrained algorithm can be used to get from t to $t-1$.

$$B. \quad x_t = l_t$$

The lower constraint is binding.

This implies $\rho_t^* = 0$, since $x_t = l_t$, therefore $x_t \neq u_t$ and $(u_t - x_t)\rho_t^* = 0$.

If the constraint is binding

$$\sigma_t^* = G_t y_{t-1} + g_t - l_t \quad (15)$$

using (11).

$$C. \quad x_t = u_t$$

The upper constraint is binding.

$$\text{This implies } \sigma_t^* = 0$$

and

$$\rho_t^* = -G_t y_{t-1} - g_t + u_t \quad (16)$$

CASE B

For case B

$$\begin{aligned} \sigma_t^* &= G_t y_{t-1} + g_t - l_t \\ \text{or } \sigma_t^* &= (C'_t H_t C_t)^{-1} (G_t y_{t-1} + g_t - l_t) \end{aligned} \quad (17)$$

Substituting this into (13)

$$\lambda_{t-1} = K_{t-1} y_{t-1} - K_{t-1} a_{t-1} + A'_t H_t (A_t + C_t G_t) y_{t-1} \quad (18)$$

$$\begin{aligned}
& + A'_t H_t (B_t z_t + C_t g_t) \\
& - A'_t H_t C_t (G_t y_{t-1} + g_t - l_t) \\
& - A'_t h_t \\
\lambda_{t-1} & = K_{t-1} y_{t-1} - K_{t-1} a_{t-1} + A'_t H_t A_t y_{t-1} + A'_t H_t C_t G_t y_{t-1} \\
& + A'_t H_t B_t z_t + A'_t H_t C_t g_t \\
& - A'_t H_t C_t G_t y_{t-1} - A'_t H_t C_t g_t + A'_t H_t C_t l_t - A'_t h_t \\
\lambda_{t-1} & = K_{t-1} y_{t-1} - K_{t-1} a_{t-1} + A'_t H_t A_t y_{t-1} + A'_t H_t B_t z_t \\
& + A'_t H_t C_t l_t - A'_t h_t \\
\lambda_{t-1} & = H_{t-1}^* y_{t-1} - h_{t-1}^*
\end{aligned} \tag{19}$$

where

$$\begin{aligned}
H_{t-1}^* & = K_{t-1} + A'_t H_t A_t \\
h_{t-1}^* & = K_{t-1} a_{t-1} - A'_t H_t (B_t z_t + C_t l_t) + A'_t h_t
\end{aligned} \tag{20}$$

When comparing these with the normal recursion formula

$$\begin{aligned}
H_{t-1} & = K_{t-1} + A'_t H_t (A_t + C_t G_t) \\
h_{t-1} & = K_{t-1} a_{t-1} - A'_t H_t (B_t z_t + C_t g_t) + A'_t h_t
\end{aligned} \tag{21}$$

Notice that $x_t = l_t$ and if G_t and g_t are calculated normally and then used to calculate

$$\sigma_t^* = G_t y_{t-1} + g_t - l_t \tag{21}$$

and then if G_t is set equal to 0 and g_t is set equal to l_t , then the usual recursion formulae are used then the H_{t-1} and h_{t-1} are calculated correctly. This means that after H_t , h_t , G_t , and g_t are calculated using the normal recursion and it is found that x_t would be out of the bounds set for it, then we calculate σ_t^* and set $G_t = 0$ and $g_t = l_t$ and calculate H_{t-1} and h_{t-1} for the given x_t and G_t and g_t .

Notice that y_{t-1} has not been calculated yet and is needed to calculate ρ_t^* . If one uses the nonlinear algorithm (Chow, 1975) then an estimate of y_{t-1} is available from the last iteration. At convergence this y_{t-1} will be arbitrarily close to the "actual" y_{t-1} .

CASE C

Similarly for case C:

$$x_t = u_t$$

and

$$\rho_t^* = -G_t y_{t-1} - g_t + u_t$$

$$H_{t-1}^* = K_{t-1} + A_t' H_t A_t$$

$$h_{t-1}^* = K_{t-1} a_{t-1} - A_t' H_t (B_t z_t + C_t u_t) + A_t' h_t$$

Here again if the G_t and g_t are calculated normally then $\rho_t^* = -G_t y_{t-1} - g_t + u_t$ and then set $x_t = u_t$, $G_t = 0$ and $g_t = u_t$. Then the normal recursion formula (21) will work correctly.

AN EXAMPLE

For example, suppose we wish to constrain the instruments to be positive, $x_t \geq 0$.

$$\min(y_t - a_t)' K_t (y_t - a_t)$$

subject to

$$y_t = A_t y_{t-1} + C_t x_t + B_t z_t$$

and

$$x_t \geq 0$$

Forming the Lagrangean we get

$$L = \frac{1}{2} \sum_{t=1}^T (y_t - a_t)' K_t (y_t - a_t) - \sum_{t=1}^T \lambda_t' (y_t - A_t y_{t-1} - C_t x_t - B_t z_t) - \sum_{t=1}^T \rho_t x_t$$

$$\frac{\partial L}{\partial y_t} = K_t (y_t - a_t) - \lambda_t + A_{t+1}' \lambda_{t+1} = 0 \quad (1)$$

$$\frac{\partial L}{\partial x_t} = C_t' \lambda_t - \rho_t = 0 \quad (2)$$

$$\frac{\partial L}{\partial \lambda_t} = y_t - A_t y_{t-1} - C_t x_t - B_t z_t = 0 \quad (3)$$

$$\frac{\partial L}{\partial \rho_t} = -x_t \leq 0 \quad (4)$$

$$\rho_t \frac{\partial L}{\partial \rho_t} = -\rho_t x_t = 0 \quad (5)$$

Using the example in Chow (1975) we begin with period T

$$\lambda_T = K_T y_T - K_T a_T + A'_{T+1} \lambda_{T+1} \quad \text{using} \quad (1)$$

Setting $H_T = K_T$ and $h_T = K_T a_T$

$$\lambda_T = H_T y_T - h_T \quad (6)$$

$$C'_T \lambda_T - \rho_T = 0 \quad (2)$$

$$C'_T (H_T y_T - h_T) - \rho_T = 0 \quad \text{using (2) and} \quad (6)$$

$$C'_T (H_T A_T y_{T-1} + H_T C_T x_T + H_T B_T z_T - h_T) - \rho_T = 0 \quad \text{using} \quad (3)$$

Solving for x_T

$$C'_T H_T A_T y_{T-1} + C'_T H_T C_T x_T + C'_T H_T B_T z_T - C'_T h_T - \rho_T = 0$$

$$C'_T H_T C_T x_T = -C'_T H_T A_T y_{T-1} - C'_T H_T B_T z_T + C'_T h_T + \rho_T$$

or

$$x_T = G_T y_{T-1} + g_T + \rho_T^* \quad (7)$$

where

$$G_T = -(C'_T H_T C_T)^{-1} C'_T H_T A_T$$

$$g_T = -(C'_T H_T C_T)^{-1} C'_T (H_T B_T z_T - h_T)$$

$$\rho_T^* = (C'_T H_T C_T)^{-1} \rho_T$$

Solving for y_T as a function of y_{T-1}

$$y_T = (A_T + C_T G_T) y_{T-1} + B_T z_T + C_T g_T + C_T \rho_T^*$$

$$\lambda_T = H_T (A_T + C_T G_T) y_{T-1} + H_T (B_T z_T + C_T g_T) + H_T C_T \rho_T^* - h_T \quad \text{using} \quad (6)$$

Substitute this into (1)

$$K_{t-1} y_{t-1} - K_{t-1} a_{t-1} - \lambda_{t-1} + A'_t \lambda_t = 0$$

$$\lambda_{t-1} = K_{t-1} y_{t-1} - K_{t-1} a_{t-1} + A'_t \lambda_t = 0$$

$$\lambda_{t-1} = K_{t-1} y_{t-1} - K_{t-1} a_{t-1} + A'_t H_t (A_t + C_t G_t) y_{t-1} + A'_t H_t \quad (8)$$

$$(B_t z_t + C_t g_t) + A'_t H_t C_t \rho_t^* - A'_t h_t$$

Or

$$\lambda_{t-1} = H_{t-1}y_{t-1} - h_{t-1} + A'_t H_t C_t \rho_t^*$$

where

$$H_{t-1} = K_{t-1} + A'_t H_t (A_t + C_t G_t) \quad (9)$$

$$h_{t-1} = K_{t-1} a_{t-1} - A'_t H_t (B_t z_t + C_t g_t) + A'_t h_t \quad (10)$$

Using (5) the problem breaks down into two cases:

1) A. Constraint $x_t \geq 0$ is binding

$$\rightarrow x_t = 0 \text{ and } \rho_t^* = -G_t y_{t-1} - g_t \text{ using (7)}$$

2) B. Constraint $x_t \geq 0$ is not binding

$$\rightarrow \rho_t = 0 \text{ and } x_t \geq 0$$

In case B $\rho_t = 0$ reduces to Chow's algorithm

In case A

Substituting $\rho_t^* = -G_t y_{t-1} - g_t$ into (8), or $\rho_t = -(C'_t H_t C_t)^{-1}(G_t y_{t-1} + g_t)$.

we get

$$\begin{aligned} \lambda_{t-1} &= K_{t-1}y_{t-1} - K_{t-1}a_{t-1} + A'_t H_t (A_t + C_t G_t)y_{t-1} + A'_t H_t \\ &\quad (B_t z_t + C_t g_t) + A'_t H_t C_t (-G_t y_{t-1} - g_t) - A'_t h_t \\ &= K_{t-1}y_{t-1} - K_{t-1}a_{t-1} + A'_t H_t A_t y_{t-1} + A'_t H_t B_t z_t \\ &\quad + A'_t H_t C_t G_t y_{t-1} + A'_t H_t C_t g_t - A'_t H_t C_t G_t y_{t-1} - A'_t H_t C_t g_t - A'_t h_t \\ \lambda_{t-1} &= K_{t-1}y_{t-1} - K_{t-1}a_{t-1} + A'_t H_t A_t y_{t-1} + A'_t H_t B_t z_t - A'_t h_t \\ &= H_{t-1}^* y_{t-1} - h_{t-1}^* \end{aligned}$$

where

$$H_{t-1}^* = K_{t-1} + A'_t H_t A_t$$

$$h_{t-1}^* = K_{t-1} a_{t-1} - A'_t H_t B_t z_t + A'_t h_t$$

Chow (1975) shows that the two Ricatti difference equations (9) and (10) can be written as

$$H_{t-1} = K_{t-1} + (A_t + C_t G_t)' H_t (A_t + C_t G_t) \quad (11)$$

$$h_{t-1} = K_{t-1}a_{t-1} + (A_t + C_t G_t)^{-1}(h_t - H_t B_t z_t) \quad . \quad (12)$$

for case B

Notice that if *Case A* applies, i.e. $x_t = 0$ and the constraint is binding the recursion formulae are

$$\begin{aligned} H_{t-1}^* &= K_{t-1} + A_t' H_t A_t \\ h_{t-1}^* &= K_{t-1}a_{t-1} + A_t'(h_t - H_t B_t z_t) \end{aligned}$$

These are exactly what (11) and (12) reduce to when G_t and g_t are set = 0. Also, since each period can be solved separately (from dynamic programming), the solution procedure for the optimal problem subject to $x \geq 0$ can be implemented as follows.

SOLUTION PROCEDURE

Steps

1. Proceed as if x_t is unconstrained
2. Calculate H_t, h_t
then G_t, g_t
then calculate x_t using last iterations y_{t-1} .
3. If x_t is positive, proceed as in Chow (1975) to t-1
if x_t is negative, set $x_t = 0, \rho_t = -G_t y_{t-1} - g_t$
then set $G_t = 0$ and $g_t = 0$
then proceed as in Chow (1975) to t-1.
4. Start at step 1 with a new period t-1

Note 1: This allows not only x_{t-1} to change since y_t and y_{t-1} may be different, but also allows the coefficient feedback matrices G_t and g_t to change correctly knowing that $x_t \geq 0$

Note 2: For x_t a vector only the rows of G_t and g_t corresponding to negative values are set equal to zero.

BIBLIOGRAPHY

- Chow, G.C., Analysis and Control of Dynamic Economic Systems, John Wiley and Sons, New York, 1975.
- Tan, K.C., Optimal Control of Linear Econometric Systems with Linear Equality Constraints on the Control Variables, International Economic Review, Vol. 20, No. 1, Feb. 1979.